

$B(\text{Cl})$  respectively become  $1.85 \pm 0.14$  and  $1.40 \pm 0.08$  Å<sup>2</sup> for measurement No. 1 and  $1.75 \pm 0.11$  and  $1.33 \pm 0.06$  Å<sup>2</sup> for measurement No. 2. The corresponding values of  $R$  become 0.043 for measurement No. 1 and 0.049 for measurement No. 2. It is considered that use of  $\beta$ -filters only, together with fixed counter apertures, results in systematic deviations in the intensity measurements. The  $F_{\text{meas}}$  in Tables 2 and 4 should hence be regarded as illustrative of the evaluation method, and not as error-free data.

In summary, it is suggested that the criteria developed in this paper be applied to each diffractometer system built. Analysis of the results thus obtained should enable us to evaluate each system, not only in comparison with other systems, but also on an absolute basis.

It is a pleasure to thank J. L. Bernstein for his careful operation of PEXRAD and for the many computations performed on the IBM 7090.

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## Single-Crystal Diffractometry: The Improvement of Accuracy in Intensity Measurements

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Some important experimental factors are considered which must be chosen so as to satisfy a valid concept of integrated reflection intensity when using an incident X-ray beam taken directly off the target of the X-ray tube. The general superiority of the  $2\theta$  scan over the  $\omega$  scan is demonstrated by an analysis of pertinent factors. A basic reason is that spectral dispersion can be readily allowed for in the  $2\theta$  scan by proper choice of the scan range, whereas in the  $\omega$  scan it must be accomplished by regulation of the receiving aperture. Thus the  $\omega$ -scan technique demands excessively wide apertures at large  $\theta$ 's when  $\beta$ -filtered radiation is employed and over very large ranges of  $\theta$  when balanced filters are used. Very feeble reflections can often be measured more accurately by taking peak ( $I_p$ ) rather than integrated ( $I_i$ ) intensities, but such  $I_p$  data must be transformed into the equivalent  $I_i$ 's by means of empirical correction curves for the crystal concerned. Other practical recommendations are made, and the results of five structure refinements are presented to illustrate the efficacy of the  $2\theta$ -scan technique.

### 1. Introduction

The success of diffractometric intensity measurements depends upon adherence to a valid working concept of integrated reflection intensity,  $I_i(hkl)$ . When the incident beam is taken directly off the target of the X-ray tube, a satisfactory concept can be based upon the experimental requirement that every point on the crystal be enabled to 'view' every point on the focal spot. It follows that when a crystal of negligible absorption is turned through the angular reflecting range

of a set of planes ( $hkl$ ) corresponding to a characteristic wavelength  $\lambda_0$ , every volume element contributes with equal weight to the overall (integrated) reflection intensity.

The present paper is devoted to a consideration of the important experimental factors which make it possible to conform in actual practice to the above definition of  $I_i$ . A working concept based on crystal-monochromatized radiation is more difficult to define and is not proposed. We devote our attention to three- or four-circle diffractometers of the normal-beam



Provided  $\gamma_R$  is sufficiently large, the  $\omega$  scan is thus capable of revealing segments of the continuous radiation streak lying along the diametral row line on either side of the node ( $hkl$ ). Under these conditions, just as in the  $2\theta$  scan, the intensity components (1), (2), (3) and (5) can be removed from the overall integrated reflection intensity by subtracting the background measured *on top of the general radiation streak*, say, at points  $b_1$  and  $b_2$  in Fig. 3(a). Although this method can be effective when judiciously applied (for example, Fischer & Hahn, 1961), it is subject to more or less serious errors if the receiving aperture

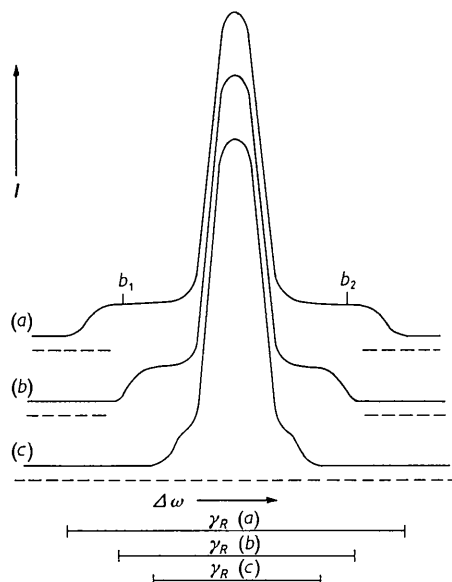


Fig. 3. Intensity profiles obtained by the  $\omega$ -scan technique showing effects of (a) wide, (b) medium, (c) narrow receiving apertures.

is too narrow. Specifically, since the width of the reflection profile at small to moderate values of  $\theta$  is principally due to the X-ray source, it is necessary that  $\gamma_R$  be not smaller than about  $3\gamma_x$ ,  $\gamma_x$  being the overall angular width of the X-ray source profile. Thus for  $\gamma_x = 0.7^\circ$ ,  $\gamma_R$  should certainly be no smaller than  $2.0^\circ$ . Figs. 3(b) and (c) illustrate the disappearance of the continuous radiation profile as  $\gamma_R$  is reduced.

Because of the  $\tan \theta$  dependence of spectral dispersion, at small Bragg angles the general radiation hump associated with a r.l. node ( $hkl$ ) tends to contract within the main reflection profile and be lost to sight. This phenomenon is observable with either the  $2\theta$  or  $\omega$  scan, and it is accentuated when  $\gamma_x$  and/or the direct lattice translations are large. Although in these circumstances the continuous-radiation background cannot be measured directly, a method of circumventing this difficulty when employing the  $2\theta$ -scan technique is described in § 7.

#### 4. Use of Ross balanced filters

Subject to rather stringent limitations, Ross balanced filters (Ross, 1929), most effectively employed in conjunction with pulse-height discrimination, can be used with the  $\omega$  scan to remove the contributions of extraneous wavelengths from the experimental values of  $I_i(hkl)$ . The first limitation is a consequence of the fact that spectral dispersion varies as  $\tan \theta$ . As a result, the angular width of the pass band, although practically small at sufficiently small Bragg angles, tends to become prohibitively large as  $\theta$  increases. Whereas in the  $2\theta$  scan spectral dispersion effects, including the pass band of a balanced-filter pair, can be encompassed by appropriately choosing the angular scan range, in the  $\omega$  scan this can be accomplished only by adjusting the width of the receiving aperture. As Table I shows, for the relatively favorable case of the pair Zr and Y used with Mo radiation, the pass band range already exceeds  $5^\circ$  at  $2\theta = 80^\circ$ , so that with the best scintillation counters currently available it is not feasible to make measurements above  $2\theta = 60$  or  $70^\circ$ . For nearly all other balanced-filter pairs the angular widths of the pass bands at a given value of  $2\theta$  are much larger (Furnas, 1957, Table VII-2).

Table I. Angular pass bands ( $\Delta 2\theta$ ) for balanced filters of Zr and Y

$2\theta$	$\Delta 2\theta$	K edge of Zr $2\theta_{\min}$	K edge of Y $2\theta_{\max}$
$20^\circ$	$1.10^\circ$	$19.46^\circ$	$20.56^\circ$
$60$	$3.60$	$58.23$	$61.83$
$80$	$5.23$	$77.43$	$82.66$
$100$	$7.44$	$96.39$	$103.83$

The second limitation on the use of Ross filters arises from the fact that parasitic and thermal diffuse scattering, being due very largely to  $K\alpha$  radiation, are passed by the filter pair, as illustrated in Fig. 4. From the difference between the integrated intensities passed by the  $\beta$  and  $\alpha$  filters it is necessary to determine and subtract the integrated intensity represented by the hatched zone of the figure. In order to do this it is necessary to make the four background measurements  $(b_\beta)_1$ ,  $(b_\beta)_2$ ,  $(b_\alpha)_1$  and  $(b_\alpha)_2$ . This procedure is tedious in contrast to the simpler  $2\theta$  scan with two background measurements. When many hundreds or even some thousands of reflections are to be measured, as is to be expected for the majority of present-day structure determinations, the balanced-filter technique is not generally acceptable.

An additional weakness of the  $\omega$ -scan-balanced-filter technique may be cited, namely, that the mandatory use of a wide receiving aperture at larger Bragg angles entails the reception of an unduly large amount of background scatter, which severely curtails

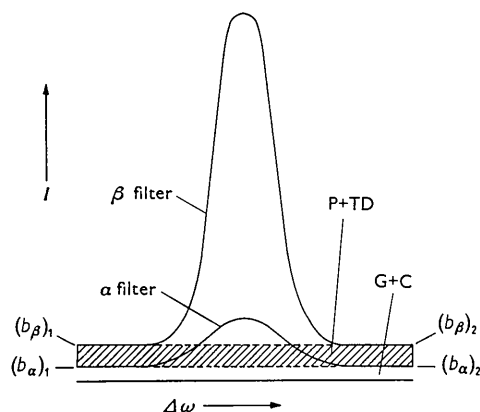


Fig. 4. Background intensity components transmitted by the  $\alpha$  and  $\beta$  filters of a Ross balanced pair. The angular width of the filter pass band and  $\gamma_R$  are both larger than the range of  $\Delta\omega$  shown. P+TD=parasitic plus thermal diffuse scatter. G+C=general radiation plus Compton scatter.

the accuracy with which weak reflections can be measured because of adverse counting statistics. In spite of the several deficiencies just described, the  $\omega$ -scan-balanced-filter method has been employed successfully in studies by Young (1962) and by Verschoor & Keulen (1963).

### 5. Receiving aperture dimensions and scan range

The authors have previously given expressions (AS, Appendix D) for the vertical (or axial) and horizontal (or equatorial) dimensions of the receiving aperture. Although the correct choice of both dimensions is essential to the realization of valid intensity measurements, in the present treatment we confine ourselves to a discussion of the equatorial dimension. In defining the minimum width,  $(\lambda_R)_{\min}$ , pertinent to the  $\omega$  scan with  $\beta$  filter, we shall at first neglect the requirement voiced in § 3 that  $\gamma_R \geq 3\gamma_x$  in order to reveal adequately the continuous-radiation background. The values of  $(\gamma_R)_{\min}$  appropriate to the  $2\theta$  and  $\omega$  scans are then functions of the inherent reflecting range of the crystal ( $\gamma_m$ ), spectral dispersion on the  $\theta$  scale ( $\gamma_\lambda$ ), angular diameter ( $\gamma_c$ ) of the crystal subtended at the X-ray source, and angular width ( $\gamma_x$ ) of the X-ray source subtended at the crystal. Recently the authors have revised the original expressions (Alexander & Smith, 1964) by incorporating more accurate terms in  $\gamma_c$  according to a suggestion of Burbank (1964). Most commonly the source-to-crystal distance is set equal to the crystal-to-receiver distance, in which case the equations reduce to:

$$2\theta \text{ scan, } (\gamma_R)_{\min} = 2\gamma_m + \gamma_x + 2\gamma_c \sin \theta. \quad (2)$$

$$\omega \text{ scan, } (\gamma_R)_{\min} = 2\gamma_\lambda(\theta) + \gamma_x + 2\gamma_c \cos \theta. \quad (3)$$

Of the four parameters only  $\gamma_\lambda$  is  $\theta$ -dependent; it

embodies two dispersion effects, both proportional to  $\tan \theta$ : dispersion within  $K\alpha_1$  or  $K\alpha_2$  and separation of  $K\alpha_1$  and  $K\alpha_2$ . From these equations we see that spectral dispersion must be allowed for in the  $\omega$  scan by proper choice of the receiving aperture width, whereas in the  $2\theta$  scan this is accomplished by adjustment of the scan range. The situation in this respect is entirely parallel to that discussed earlier involving the wavelength pass band of a balanced-filter pair.

The  $2\theta$  scan range may be appropriately set equal to the sum of two terms, the first a constant  $(\Delta 2\theta)_0$  and the second proportional to  $\tan \theta$ , which is the term  $2\gamma_\lambda(\theta)$  of equation (3). Now  $(\Delta 2\theta)_0 = 2\gamma_m + 2\gamma_x + 2\gamma_c$ , while  $2\gamma_\lambda(\theta)$  is difficult to evaluate because of the indefinite angular width of the Cauchy-like spectral line profile. However, in practice it may be set equal to the angular separation of the  $K\alpha$  doublet plus ten times the angular width of the  $K\alpha_2$  line at half-maximum intensity.\* This gives in degrees for Cu  $K\alpha$  radiation  $2\gamma_\lambda = 0.86 \tan \theta$  and for Mo  $K\alpha$   $1.00 \tan \theta$ . Letting  $2\gamma_m$ ,  $2\gamma_x$ , and  $2\gamma_c$  have representative values of  $0.3^\circ$ ,  $1.4^\circ$ , and  $0.1^\circ$  respectively, we obtain the following  $2\theta$  scan ranges:

$$\text{Cu } K\alpha, \Delta 2\theta = 1.80 + 0.86 \tan \theta \text{ degrees.} \quad (4)$$

$$\text{Mo } K\alpha, \Delta 2\theta = 1.80 + 1.00 \tan \theta \text{ degrees.} \quad (5)$$

From equation (3) the necessary receiving aperture widths for the  $\omega$ -scan technique would be:

$$\text{Cu } K\alpha, (\gamma_R)_{\min} = 0.80 + 0.86 \tan \theta \text{ degrees.} \quad (6)$$

$$\text{Mo } K\alpha, (\gamma_R)_{\min} = 0.80 + 1.00 \tan \theta \text{ degrees.} \quad (7)$$

In equations (6) and (7) we have assigned to the term  $2\gamma_c \cos \theta$  of equation (3) its fixed maximum value,  $2\gamma_c$ , since it is ordinarily very small in comparison with  $2\gamma_\lambda + \gamma_x$ .

Using the representative numerical parameters of equations (4) to (7), we give in columns 2, 3, 4 and 5 of Table 2 the required receiving aperture widths for the  $\omega$  scan and  $2\theta$  scan ranges appropriate to Cu  $K\alpha$  and Mo  $K\alpha$  radiations for Bragg angles ranging from  $10$  to  $80^\circ$ . In practice it suffices to increase  $\Delta 2\theta$  and  $(\gamma_R)_{\min}$  stepwise over the experimental range of  $\theta$  involved. An inspection of Table 2 shows that whereas it is possible to attain all the required  $2\theta$ -scan ranges in practice, the receiving apertures required in the  $\omega$ -scan technique at large  $\theta$ 's are impossibly wide in the present stage of development of counters. Furthermore, even when realizable in experiment, the wider apertures called for in the table would sharply reduce the sensitivity of the apparatus to weak reflections, as was pointed out in connection with balanced filters.

To this point in the analysis of  $\gamma_R$  for the  $\omega$  scan

\* Previously the authors suggested five times the width of either  $K\alpha$  component at half-maximum intensity (AS), but further consideration has shown a larger scan range to be desirable.

Table 2. Minimum receiving aperture widths,  $(\gamma_R)_{\min}$ , for the  $\omega$ -scan and minimum  $2\theta$ -scan ranges,  $(\Delta 2\theta)_{\min}$ , for typical experimental conditions

$\gamma_m = 0.15^\circ$ ,  $\gamma_x = 0.7^\circ$ ,  $\gamma_c = 0.05^\circ$   
 $2\gamma_\lambda = 0.86 \tan \theta$  and  $1.00 \tan \theta$  for Cu  $K\alpha$  and Mo  $K\alpha$  resp.

$\theta$	$(\gamma_R)_{\min}$ for $\omega$ scan					
	$(\Delta 2\theta)_{\min}$ for $2\theta$ scan (equations (4) and (5))		(equations (6) and (7))		(proper portrayal of background)	
	Cu $K\alpha$	Mo $K\alpha$	Cu $K\alpha$	Mo $K\alpha$	Cu $K\alpha$	Mo $K\alpha$
10°	1.95°	1.98°	0.95°	0.98°	2.00°	2.00°
20	2.11	2.16	1.11	1.16	2.00	2.00
30	2.30	2.38	1.30	1.38	2.00	2.00
40	2.52	2.64	1.52	1.64	2.00	2.00
50	2.83	2.99	1.83	1.99	2.00	2.00
60	3.30	3.53	2.30	2.53	2.30	2.53
70	4.17	4.55	3.17	3.55	3.17	3.55
80	6.70	7.47	5.70	6.47	5.70	6.47
(1)	(2)	(3)	(4)	(5)	(6)	(7)

we have ignored the constraint  $\gamma_R \geq 3\gamma_x$  imposed by the need to portray the background properly. If this practical consideration is now allowed to take precedence in the calculation of the numerical values of Table 2, columns 4 and 5 must be replaced by 6 and 7, in which  $\gamma_R$  never assumes values less than  $2^\circ$ . The absence of a  $\gamma_m$  term in equation (3) discloses one circumstance apparently favorable to the  $\omega$  scan, namely, its application to the measurement of a highly mosaic crystal. Nevertheless, even with  $\gamma_m$  as large as  $1^\circ$ , if we assign  $\gamma_x$ ,  $\gamma_\lambda$ , and  $\gamma_c$  typical values of  $0.7^\circ$ ,  $0.2^\circ$ , and  $0.05^\circ$  respectively,  $(\gamma_R)_{\min}$  for the  $2\theta$  scan is  $2.8^\circ$ , whereas for the  $\omega$  scan it is not less than  $2.0^\circ$  for the practical reason just explained. Certainly this is not a great disparity in favor of the  $\omega$  scan. It is true that some alleviation would result for both the  $2\theta$ - and  $\omega$ -scan techniques with  $\beta$  filtration if the X-ray source dimension were reduced. Other factors being favorable, however, it would probably be advantageous to measure the reflection intensities

of such a highly mosaic crystal by the  $\omega$ -scan-balanced-filter technique.

Table 3 summarizes the relative merits of three scanning techniques: (1) the  $2\theta$  scan with  $\beta$  filter, (2) the  $\omega$  scan with  $\beta$  filter and  $(\gamma_R)_{\min} = 3\gamma_x$ , (3) the  $\omega$  scan with balanced filters and  $(\gamma_R)_{\min} = 2\gamma_\lambda + \gamma_x + 2\gamma_c$ , where  $2\gamma_\lambda$  is the angular width of the pass band on the  $2\theta$  scale. It is clear that on the basis of all the evidence examined, the  $2\theta$  scan is to be preferred for general use.

### 6. Integral versus peak intensities

The authors strongly recommend that in ordinary practice integrated intensities be measured directly, although in certain circumstances it may occasionally be advantageous to employ the stationary-crystal stationary-counter technique to measure peak intensities,  $I_p(hkl)$ . The measurement of very feeble reflections constitutes such a situation, because then  $I_p/I_b$

Table 3. Concise summary of the characteristics of the  $\omega$ - and  $2\theta$ -scan techniques

	$2\theta$ scan $\beta$ filter	$\omega$ scan $\beta$ filter $(\gamma_R)_{\min} = 3\gamma_x$	$\omega$ scan balanced filters $(\gamma_R)_{\min} = 2\gamma_\lambda^* + \gamma_x + 2\gamma_c$
1. Number of measurements required	1 scan 2 backgrounds	1 scan 2 backgrounds	2 scans 4 backgrounds
2. Elimination of wavelengths other than $\lambda_0$ from net measured value of $I_i$	satisfactory	satisfactory except at large $2\theta$ 's	satisfactory within restricted $2\theta$ range
3. Elimination of parasitic and Compton scatter	satisfactory	satisfactory	satisfactory
4. Elimination of thermal diffuse scatter	incomplete	incomplete	incomplete
5. Allowance for increase of spectral dispersion with $\theta$	satisfactory except at large $2\theta$ 's	unsatisfactory in general	unsatisfactory in general
6. Effectiveness in measuring weak intensities	satisfactory	unsatisfactory	unsatisfactory
7. Suitability for highly mosaic crystals	unsatisfactory	satisfactory	satisfactory

\*  $2\gamma_\lambda$  = angular width of pass band on  $2\theta$  scale.

is appreciably larger than  $I_i/I_b$ , resulting in better resolution of the  $(hkl)$  peak from the background. The reader is reminded that the relative standard deviation in the net intensity (above background) of the  $(hkl)$  peak is given by

$$\sigma = (N_t + N_b)^{1/2} / (N_t - N_b), \quad (8)$$

where  $N_t$  and  $N_b$  are respectively the overall counts and background counts recorded (Klug & Alexander, 1954, p. 272). However, as the authors have previously emphasized (AS) concerning the  $2\theta$  scan, only in a limited low- $2\theta$  region is  $I_p$  approximately proportional to  $I_i$ , while at larger Bragg angles the ratio  $I_i/I_p$  increases rapidly to values exceeding 1.5 times its value at  $2\theta \rightarrow 0^\circ$ . Because of variations in mosaic character from one crystal to another, it is not possible to rely upon any one calculated or experimental curve of  $I_i/I_p$  versus  $2\theta$  for the correction of  $I_p$ 's to the equivalent  $I_i$ 's, as an inspection of Fig. 5 will show. It is necessary to plot such curves directly from selected reliable reflections of the crystal concerned, making due allowance for the possible occurrence of anisotropy.

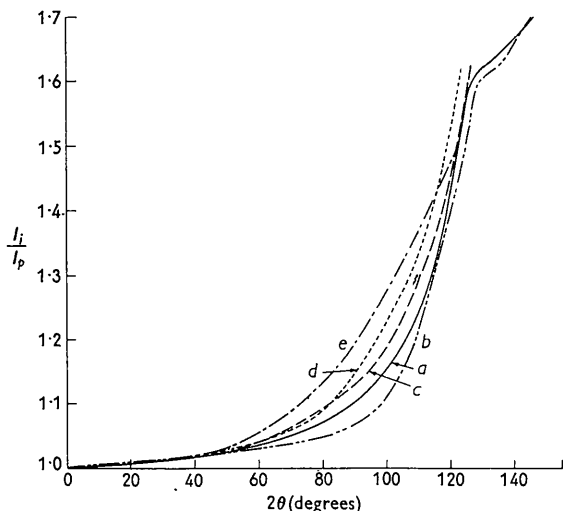
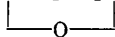


Fig. 5. Comparison of calculated and experimental curves of  $I_i/I_p$  for Cu  $K\alpha$  radiation.

- (a) Calculated, (b)  $\alpha$ -quartz, (c)  $(C_6H_5)_4Si$ ,  
 (d) cyclic tetramer  $[(CH_3)_2SiNH]_4$ ,  
 (e)  $(C_6H_5)_2SiCH_2CH_2Si(C_6H_5)_2$ .



We wish to call renewed attention to a special value of the  $I_i/I_p$  curve which has been cited earlier (AS, p. 994) in connection with the shrinkage of the general radiation hump under the reflection profile at small  $\theta$ 's. Under such circumstances the proper value of the background is that which, when subtracted from the overall experimental values of  $I_i$

and  $I_p$ , will cause the ratio  $(I_i/I_p)$  for the reflection to fall on the previously established  $I_i/I_p$  correction curve of the crystal concerned.

## 7. Further practical recommendations

(1) Possible crystal specimens should be evaluated in advance by photographic and/or counter techniques for (a) mosaic character and (b) absorption and extinction properties. Item (a) furnishes the needed value of  $\gamma_m$  for the calculation of  $(\gamma_R)_{\min}$  by equation (2) (Alexander, Smith & Brown, 1963). Item (b) involves the measurement of the variation in  $I_i$  for equivalent faces of a crystallographic form, and this information is useful as a criterion for acceptance of a given crystal or as an aid in assigning weights to the  $F_o$ 's in the crystal structure analysis.

(2) When feasible in relation to other considerations, employ a short wavelength in order to minimize the number of intensity measurements to be performed in the high- $2\theta$  region.

(3) One must always be alert to the possible presence of uneven background contours, frequently the result of interference by a neighboring reflection. Such effects will be most pronounced when a short wavelength is employed and for crystals with large unit cells. For crystals with very large cells (for example, proteins) it is helpful to employ long-wavelength radiation and to reduce  $\gamma_x$  by adjusting the target 'take-off' angle in order to improve the resolution of densely populated r.l. row lines. Excessive loss of primary beam intensity imposes an ultimate limit on the minimum acceptable value of  $\gamma_x$ .

(4) In order to compensate for possible long-period variations in primary beam intensity and monotonic decline in the reflecting power of the crystal due to radiation damage or other causes, all measured  $I_i(hkl)$  data should be referred to the intensity of a standard reflection measured at regular intervals (normally not less frequently than twice daily).

(5) When known to be significant, errors due to thermal diffuse scattering may be reduced, other considerations permitting, by reducing the temperature of the crystal during measurement.

(6) The accuracy of measurement of feeble reflections may be improved by (a) using a larger-than-average crystal, (b) minimizing parasitic scatter by careful experimental procedures and apparatus design, (c) carefully minimizing  $\gamma_R$  according to equation (2), (d) measurement of  $I_p$  and transformation to  $I_i$  by means of a correction curve.

## 8. Illustrative results

Table 4 summarizes the results of five structure refinements performed at Mellon Institute with diffractometric intensities collected by the procedures

Table 4. *Results of five structure refinements employing diffractometric intensities*

	DS=differential synthesis		LS=least squares		IA=individual anisotropic	II=individual isotropic	
Crystal	$\alpha$ -quartz		GeO <sub>2</sub>		(C <sub>6</sub> H <sub>5</sub> ) <sub>4</sub> Si	(C <sub>6</sub> H <sub>5</sub> ) <sub>4</sub> Sn	[(H <sub>3</sub> C) <sub>2</sub> SiNH] <sub>4</sub> cyclic
Radiation	Cu K $\alpha$		Mo K $\alpha$		Cu K $\alpha$	Mo K $\alpha$	Cu K $\alpha$ partial Mo K $\alpha$ partial
Method of refinement	DS and LS		LS		LS	LS	LS
Number of intensity data	112 (complete 3D)		194 (complete up to $2\theta \approx 68^\circ$ )		621 (complete 3D)	750 (partial) 350 $hk0$ , $0kl$ , and $hhl$ 400 $hkl$	934 (partial) 639 $hk0$ , $0kl$ , and $h0l$ 295 $hkl$
Number of parameters							
Positional	4		4		33*	33*	48†
Thermal	10		10		68*	68*	16†
Kind of temperature factor	IA		IA		IA	IA	II
Final $R$ (%)	DS	LS					
All $F_o$ 's	3.3	3.6	1.9	1.6‡	3.9	4.0	8.6
Non-zero $F_o$ 's	3.3	3.6	1.9	1.6‡	3.3	3.0	7.9

\* Including H atoms. † H atoms not located. ‡ Extinction assumed for three reflections.

suggested in the present paper, which made use exclusively of  $\beta$ -filtered incident X-rays. As the criterion of excellence of structural refinement we have employed the conventional reliability index,

$$R = \frac{\sum (|F_o| - |F_c|)}{\sum |F_o|}$$

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